# APPLICABILITY OF ACCELERATED TESTING CONDITIONS ON LEAD-ACID BATTERIES FOR PV Systems – Results from Cycling and Deep-discharge Laboratory Evaluation

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**ABSTRACT:** This paper reports on the applicability of accelerated lifetime procedures on solar type lead-acid batteries. Two different testing procedures were examined, namely "cycling" test and "deep discharge" test. The "cycling" test simulated battery-shedding phenomena, while the "deep discharge" test provoked rapid battery sulphation and examined the recovery capability of a battery. Seven lead-acid battery types were tested from five different manufacturers. The results showed that flooded batteries lasted approximately 500 cycles under the accelerated conditions of the "cycling" test. The equivalent cycling ability was calculated more than 1300 cycles under normal operating conditions taking into account that during its lifetime the battery's capacity does not fall below 80% of the nominal. With VRLA batteries, the final results indicated that under accelerated conditions, cycling capability was between 265 and 305 cycles for three different battery types. This corresponds to an average of 1100 cycles at room temperature. These results are satisfactory in terms of battery performance and also, in terms of validation of the applicability of the accelerated cycling procedure as a standard test in laboratories for the assessment of the lifetime of lead-acid batteries.

Keywords: Batteries - 1: Experimental Methods - 2: Evaluation - 3

# 1. INTRODUCTION

The applicability of accelerated lifetime procedures on solar type lead-acid batteries is examined in this paper. The performance evaluation procedures refer to "cycling" and "deep discharge" conditions. The work presented in this paper was co-funded by the EC within the JOULE III Programme. The relevant project was entitled, "QUALIBAT – Investigations for a QUicker Assessment of Lifetime and other key characteristics of photovoltaic BATteries", contract No JOR3-CT97-0161.

The battery tests were carried out at CRES in the period between 1998 and 2000. The Battery Laboratory is equipped with programmable cycling machines, a water bath and an environmental chamber for temperature regulation.

### 2. GENERAL TESTING CONDITIONS

The test procedures were according to the specified conditions that have been discussed and agreed by all project partners, namely GENEC, CRES, CIEMAT, OLDHAM and CHLORIDE. The varying parameters were current rate, upper and lower cut-off voltage values, charge and discharge time and temperature.

#### 2.1 Definition of a Capacity Test

Depending on the battery type, a procedure for the discharge capacity measurement at any State Of Health was developed. Assuming that before a capacity test a battery is at a high SOC level, the procedure is described step-by-step in Table 1.

Table 1. Lead-acid battery capacity test procedure

Step	Description		
1	<b>Temperature:</b> Battery at open circuit until $T = 25^{\circ}C$ .		
2	<b>Initial Discharge:</b> Discharge at a 0.1×C/10 rate until		
	1.80V per cell end voltage.		
3	Recharge (flooded)	Recharge (VRLA)	
	Constant current method.	Constant voltage method.	
	$I_{C1} = 0.25 \times C/10$ for 3h	$I_{C1} = 0.20 \times C/10$ for 20h,	
	$I_{C2} = 0.07 \times C/10$ for 7h	$V_{max} = 2.35 V dc$	
	Notes:	$I_{C2} = 0.01 \times C/10$ for 4h,	
	<ul> <li>Recharged Ah ≅120%</li> </ul>	$V_{max} = 2.35 V dc$	
	of the nominal at		
	discharge (C/10 rate).		
	<ul> <li>V<sub>max</sub> unlimited.</li> </ul>		
4	Rest Period: Battery under e	valuation at open circuit	
	condition for 24h to reach T =	$= 25^{\circ}$ C.	
5	<b>Discharge:</b> Discharge at a 0.	1×C/10 rate until 1.80V per	
	cell end voltage. Measure Ah	exchanged.	
6	<b>Conditioning:</b> Repeat steps 3 to 5 another two times		
	(three cycles in total).		
7	Capacity Measurement: Repeat steps 3 to 5. Battery		
	capacity is the Ah value of th	e 4 <sup>th</sup> cycle, Step No 5.	

#### 2.2 Selection of Battery Types

Seven lead-acid battery types were evaluated from five different manufacturers, including VRLA and flooded types. All batteries were designed and manufactured for solar stand-alone systems applications. The main characteristics of these batteries are summarised in Table 2.

Table 2. Lead-acid battery types and characteristics

Manufacturer /	Туре	Capacity Rates, [Ah]
Series		
Sonnenschein /	VRLA gel,	104(C/10), 115(C/20),
Dryfit A512	flat plate, 12V	95(C/5), 73(C/1)
Trojan / 5SH	Flooded, flat	150(C/10), 183(C/100),
	plate, 12V	165(C/20), 139(C/5)
Trojan / Pegasus	VRLA gel,	91(C10), 97(C/20),
GB12-97	flat plate, 12V	82(C/5), 65(C/1)
Trojan / T–875	Flooded, flat	139(C/10), 167(C/100),
	plate, 8V	150(C/20), 126(C/5)
Bären / Solar SGi	Flooded, flat	121(C/10), 170(C/100)
170	plate, 12V	
GNB / SUNlyte	VRLA, flat	87(C/10), 100(C/100),
12-5000X	plate, 12V	93(C/24), 72(C/5)
NWES / Solar-1	Flooded, flat	720(C/10), 879(C/100),
SO-6-85-17	plate, 2V	845(C/20), 480(C/1)

# 3. ACCELERATED CYCLING PROCEDURE

Scope of this test was to investigate a battery's ageing mechanism under accelerated cycling conditions. Fast ageing was achieved by setting the operating temperature at  $47^{0}$ C, which simulates the shedding phenomenon. Duty cycle was set at 1.5 and 3 cycles per day for the VRLA and the flooded battery types respectively. The "cycling" procedure is presented in Table 3.

Ta	ble	e 3.	Accel	lerated	cycl	ling	test	proce	dure

Step	Description			
1	<b>Temperature:</b> Battery at open circuit until $T = 47^{\circ}C$ .			
2	Discharge (flooded)	Discharge (VRLA)		
	$I_D = 0.33 \times C/10$ for 2h	$I_D = 0.22 \times C/10$ for 3h		
	<u>Notes:</u> DOD = $66\%$ of	<u>Notes:</u> DOD = $66\%$ of the		
	the C/10 rate, $V_{min} =$	$C/10$ rate, $V_{min} =$		
	(1.80÷1.90)V per cell.	(1.80÷1.90)V per cell.		
3	Recharge (flooded)	Recharge (VRLA)		
	Constant current method.	Constant voltage method.		
	$I_{C1} = 0.25 \times C/10$ for 2h	$I_{C1} = 0.19 \times C/10$ for 10h,		
	$I_{C2} = 0.071 \times C/10$ for 4h	$V_{max}=2.28V$		
		$I_{C2} = 0.01 \times C/10$ for 3h,		
		$V_{max}=2.28V$		
	<u>Notes:</u> Recharged Ah ≅	<u>Notes:</u> Recharged Ah ≅		
	(120÷125)% of the C/10	$(105 \div 125)\%$ of the C/10		
	rate, V <sub>max</sub> unlimited.	rate, $V_{max}$ =2.28V at 47°C		
		is equivalent to 2.35V at $25^{\circ}$ C.		
4	Cycling: Repeat steps 2 and	d 3 for approximately 80		
	cycles.			
	Notes: Duration of daily cycling is,			
	<ul> <li>Flooded: 2h (discharge) + 2h + 4h (recharge) =</li> </ul>			
	8h per cycle, thus 3 cy	cles per day.		
	<ul> <li>VRLA: 3h (discharge) + 10h + 3h (recharge) =</li> </ul>			
	16h per cycle, thus 1.5	cycles per day.		
5	Capacity Measurement: A	After a cycling period,		
	measure battery capacity (se	ee details in Table 1).		

Every 50 to 70 cycles, a capacity test was carried out at 25<sup>o</sup>C in order to measure the battery residual capacity. **3.1 Results from the Accelerated Cycling Test** 

The laboratory results are presented in Figures 1 to 6.



Figure 1. A512 accelerated cycling test



Figure 2. 5SH accelerated cycling test



Figure 3. Pegasus GB12-97 accelerated cycling test



Figure 4. GNB 12-5000X accelerated cycling test



Figure 5. T-875 accelerated cycling test



Figure 6. SO-6-85-17 accelerated cycling test

The experimental results indicate that flooded batteries lasted approximately 500 cycles under the accelerated conditions of the "cycling" test. The equivalent cycling ability was calculated more than 1300 cycles under normal operating conditions taking into account that during its lifetime the battery's capacity does not fall below 80% of the nominal. With VRLA batteries, cycling capability was between 265 and 305 cycles for three different battery types under accelerated lifetime conditions. This corresponds to an average of 1100 cycles at room temperature. These results are satisfactory in terms of battery performance and also, in terms of validation of the applicability of the accelerated cycling procedure as a standard test in laboratories for the assessment of the lifetime of lead-acid batteries.

#### 4. ACCELERATED DEEP DISCHARGE TEST

Scope of this test was to examine the effect of deep discharge, and thus sulphation, on lead-acid battery performance. The accelerated "deep discharge" procedure was achieved by setting the batteries at extremely low state of charge for a long period. A detailed description of this procedure is presented in Table 4.

Step	Description			
1	Battery Conditioning and Initial Capacity Test:			
	Charge and discharge rates are according to the battery			
	type (flooded or VRLA), see Table 1. Capacity			
	measurement in cycle 4 at 25°C temperature.			
2	Deep Discharge Period 1: Each deep discharge period			
	consists of 4 cycles. Test temperature = $25^{\circ}$ C.			
2a	<b>Cycle 1:</b> Discharge with 0.1×C/10 rate until battery			
	voltage reaches 1.80V per cell.			
2b	<b>Complete Discharge:</b> Connect a resistive load of $1\Omega$			
	per cell, i.e. $6\Omega$ for 12V, across the battery poles to			
	reach extremely deep discharge. Step period = 28 days.			
2c1	Re-charge for 96h with upper voltage limit 2.40V per			
	cell for both flooded and VRLA battery types. The			
	$0.1 \times C/10$ recharge rate is recommended.			
	Note: no limitation in Ah charged is set in this step.			
2c2	Instead of 2c1, an alternative procedure is suggested.			
	Recharge an amount of 1.5×C/10 Ah of the nominal			
	capacity, with upper voltage limit 2.40V per cell for			
	both flooded and VRLA battery types. Recharge rate			
	may not be set. If not free, the C/10 rate is suggested.			
3	Deep Discharge Cycles 2, 3, 4: Repeat the procedure			
	of step No 2 three times. Note: each discharge carried			
	out in 2a is an indication of the battery capacity.			
4	Capacity Test: Capacity test procedure, see Table 1.			
5	Deep Discharge Periods: Repeat steps 2 and 3.			
6	Repeat steps 4 and 5 until the battery end of life.			

From the procedure described above it is noticed that, following a full recharge regime, the deep discharge condition was repeated four times before a capacity test.

**4.1 Results from the Accelerated Deep Discharge Test** Four batteries were evaluated under "deep discharge" conditions. The laboratory results are presented in Figures 7 to 10.



Figure 7. SGi 170 accelerated deep discharge test



Figure 8. Pegasus GB12-97 accelerated deep discharge test



Figure 9. GNB 12-5000X accelerated deep discharge test



Figure 10. T-875 accelerated deep discharge test

Concerning the recharge methodology, the initial procedure described in step 2c1, Table 4, was modified as it was proven that the expected accelerated battery ageing due to high sulphation was prevented. In fact, with 96h recharge, batteries were de-sulphated during charging as positive energy transfer was in the order of 3 to 6 times more than the nominal C/10 capacity. Although this is a very useful practice for conditioning lead-acid batteries in real PV stand-alone applications, the objective to establish a quick evaluation methodology was not satisfied and excessive recharge was replaced by an energy transfer of exactly  $1.5 \times C/10$  Ah, see step 2c2.

The results show that the batteries selected have very good capacity recovery characteristics from long deep discharge conditions.

### 5. CONCLUSIONS

Two methodologies for quick evaluation of the performance of lead-acid batteries were investigated in this paper. In particular:

- Accelerated "cycling" test, simulating the shedding ageing mechanism.
- "Deep discharge" test, simulating sulphation of the plates.

Each of the two procedures was described in detail for both flooded and VRLA battery types. The experimental activities were undertaken in the Battery Laboratory of CRES and the results indicated that all batteries had satisfactory performance under accelerated cycling conditions. In terms of the applicability of the accelerated cycling procedure, the results were coherent and thus, such conditions were validated and can be used as a standard test in laboratories for quick assessment of the lifetime of lead-acid batteries. The applicability of the "deep discharge" methodology was also investigated and certified for by evaluating 4 batteries in the laboratory.