

**Gróf Gyula**

**Napkollektorok Energetikai  
értékelése**

**Energy assessment of the solar  
collectors**

# **Energetikai értékelés**

## **Energy Assessment**

- **Mit értünk ez alatt? What does it mean?**

**=**

**Technikai + Gazdasági**

**Technical + Economical**

**Szemponrendszer**

**Point of view**

**⇒ Optimum**

# **Kihez szól? Who is the listener?**

- **Felhasználók (nem szakmai közönség)**
- **Users (non specialists)**
- **Szakmai közönség (specialists):**
  - Tervezők (Designers)**
  - Installációs szakemberek**
  - Fejlesztők (Developers)**
  - ...**

# **Technikai szempontok:**

**(Technical aspects)**

- **Funkcionális megfeleléség (functions)**
- **Termodinamikai megfeleléség (thermodynamics)**
- **Élettartam (life cycle)**
- **Környezeti hatások (environmental impacts)**
- **...**

**Szabványosított minősítési eljárások!**  
**(standards)**



**SRCC STANDARD  
100-08**

**TEST METHODS  
AND MINIMUM STANDARDS  
FOR CERTIFYING  
SOLAR COLLECTORS**

**February 2008**

**INTERNATIONAL  
STANDARD**

**IEC  
61215**

Second edition  
2005-04

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**Crystalline silicon terrestrial  
photovoltaic (PV) modules –  
Design qualification and type approval**

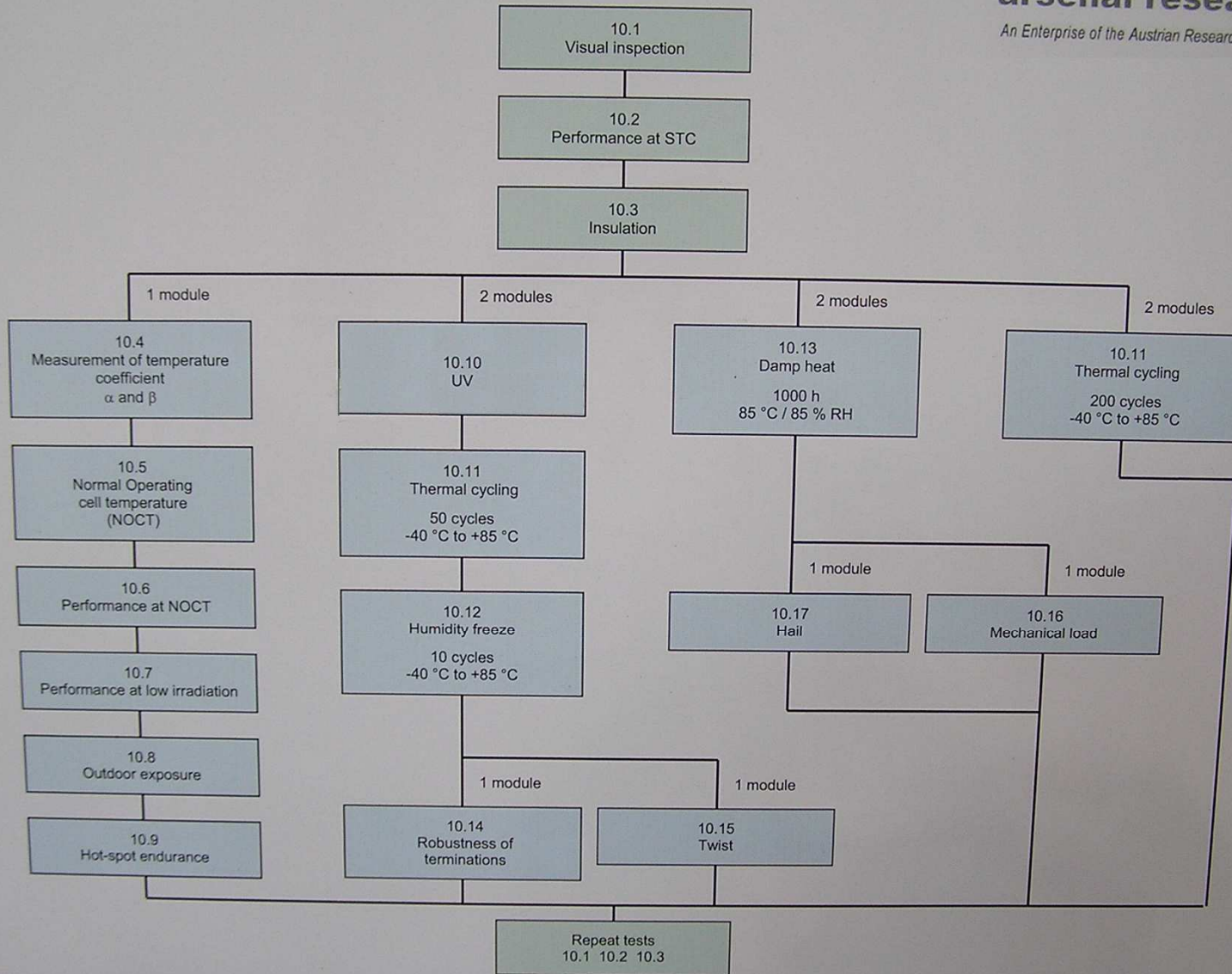
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Reference number  
IEC 61215:2005(E)

# Qualification test sequence according to EN 61215

7 test modules + 1 control module





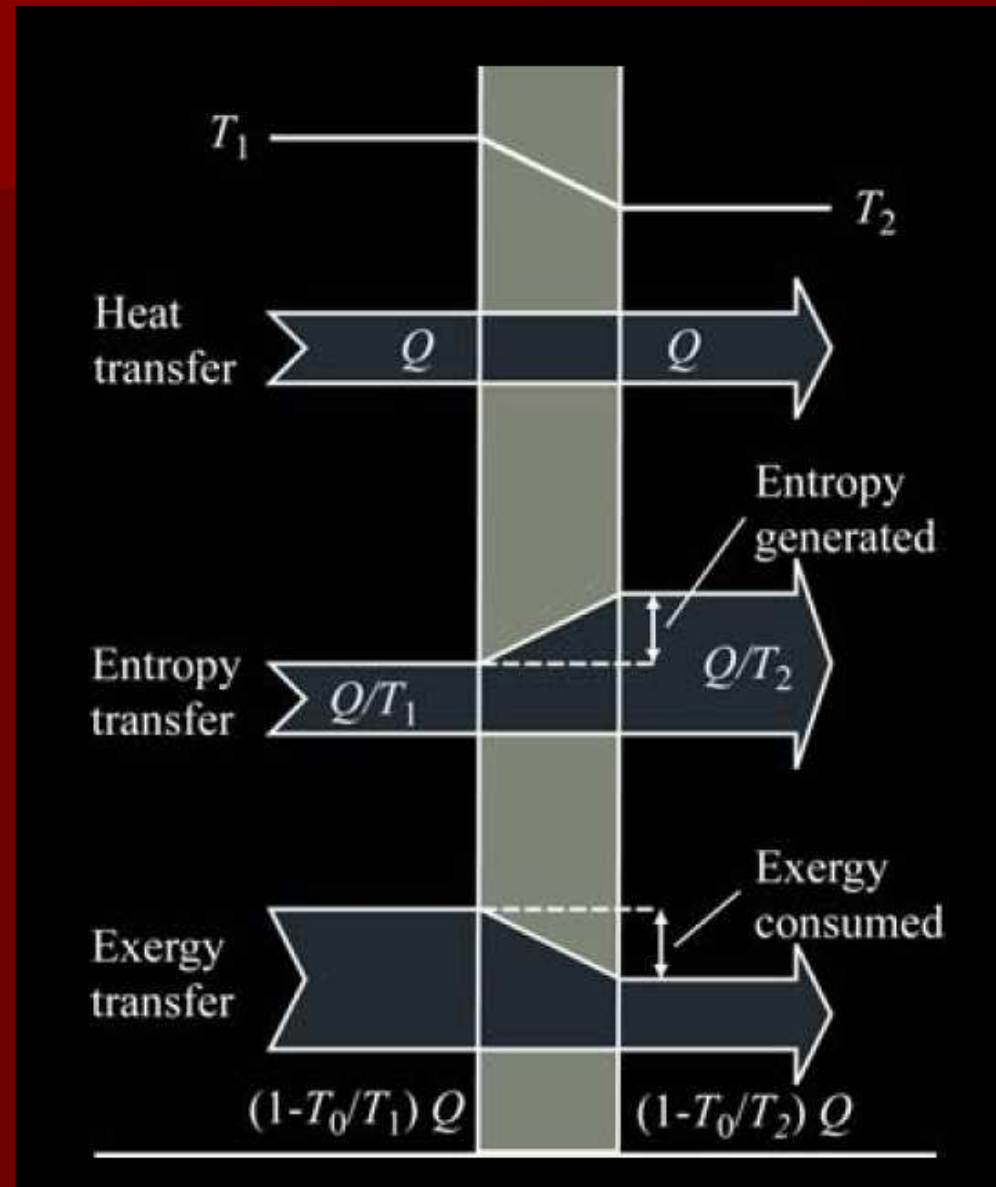
# Kollektor értékelés termodinamikai lehetőségei:

- Hőmérséklet szemlélet
- Energia szemlélet
- Entrópia szemlélet
- Exergia szemlélet

Cél: meghatározni az energia átalakítás hatékonyságát  
veszteségeket (mennyiség, minőség)  
utalni a gazdaságosságra



# Characterization of the heat transport:



# Temperature method

- optimal temperature for getting power from a heat source -

$f(T_f, T_h)$  characteristic function of heat source

$g(T_h, T_o)$  function of use of energy

$$\frac{\partial [f(T_f, T_h) \cdot g(T_h, T_o)]}{\partial T_h} = 0 \rightarrow T_{h \max}$$

$$P_{\max} = f(T_f, T_{h \max}) \cdot g(T_{h \max}, T_o)$$

Problem: knowledge of the characteristic function

## Case of radiation

$$f(T, T_h) = C \cdot [T_f^4 - T_h^4] \quad g(T_h, T_o) = 1 - \frac{T_o}{T_h}$$

$$T_{h \max} = \sqrt[5]{\frac{T_o}{4} [T_f^4 + 3 \cdot T_{h \max}^4]}$$

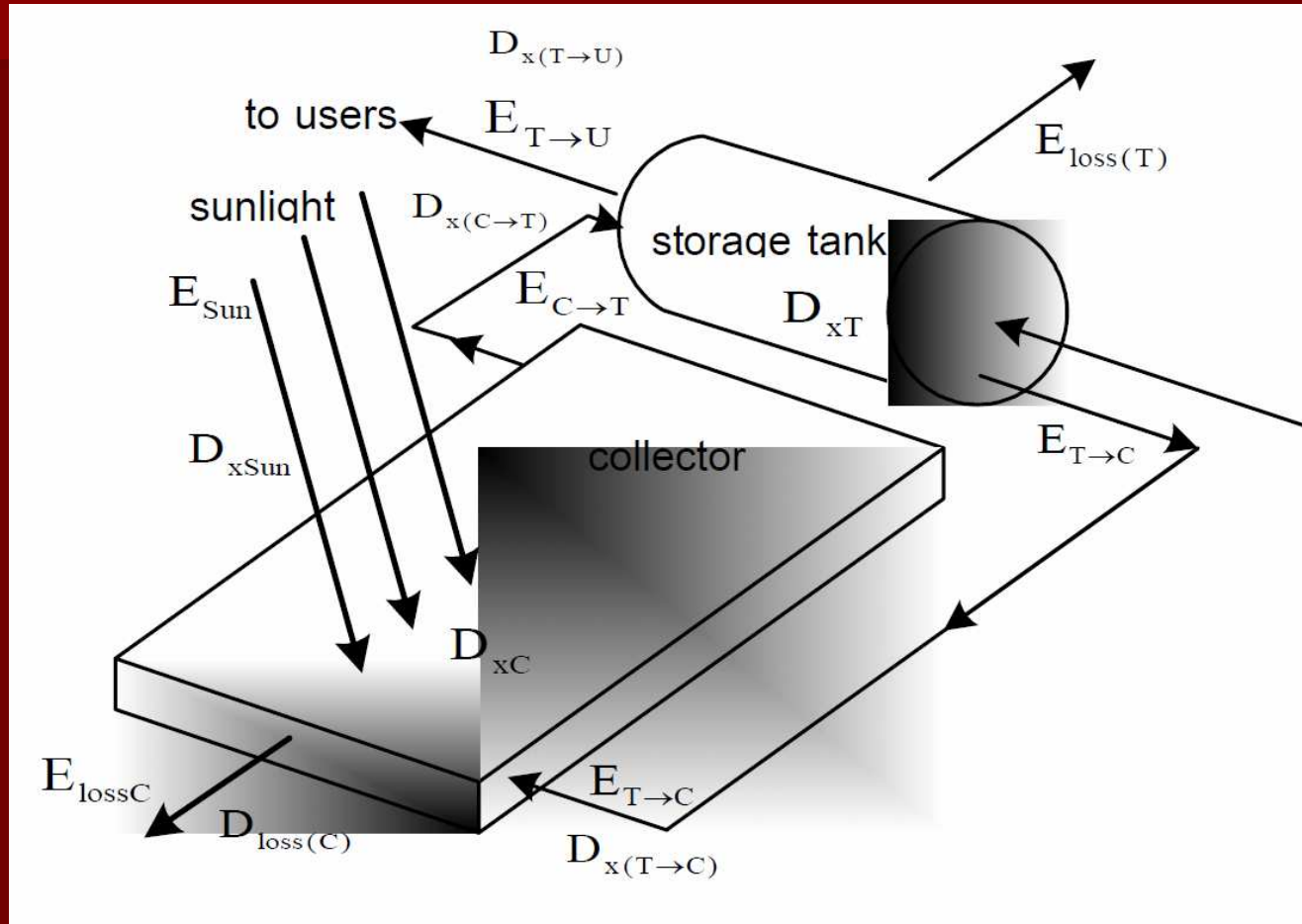
## Case of convection or conduction:

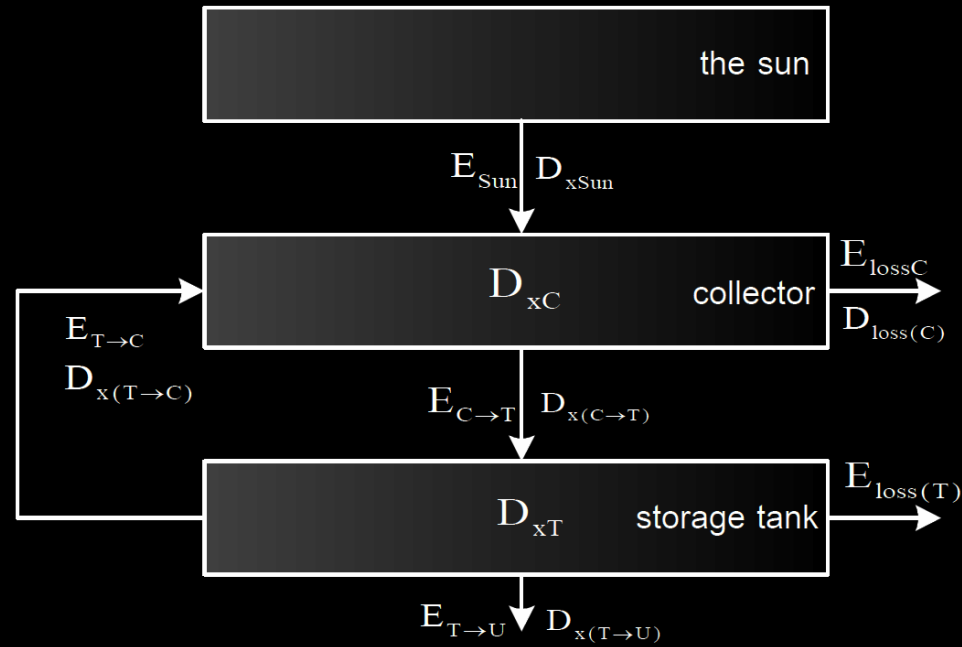
$$f(T, T_h) = C \cdot [T_f - T_h] \quad g(T_h, T_o) = 1 - \frac{T_o}{T_h}$$

$$T_{h \max} = \sqrt{[T_f \cdot T_o]}$$

# Energy method - Energia szemlélet

- application of the energy conservation -





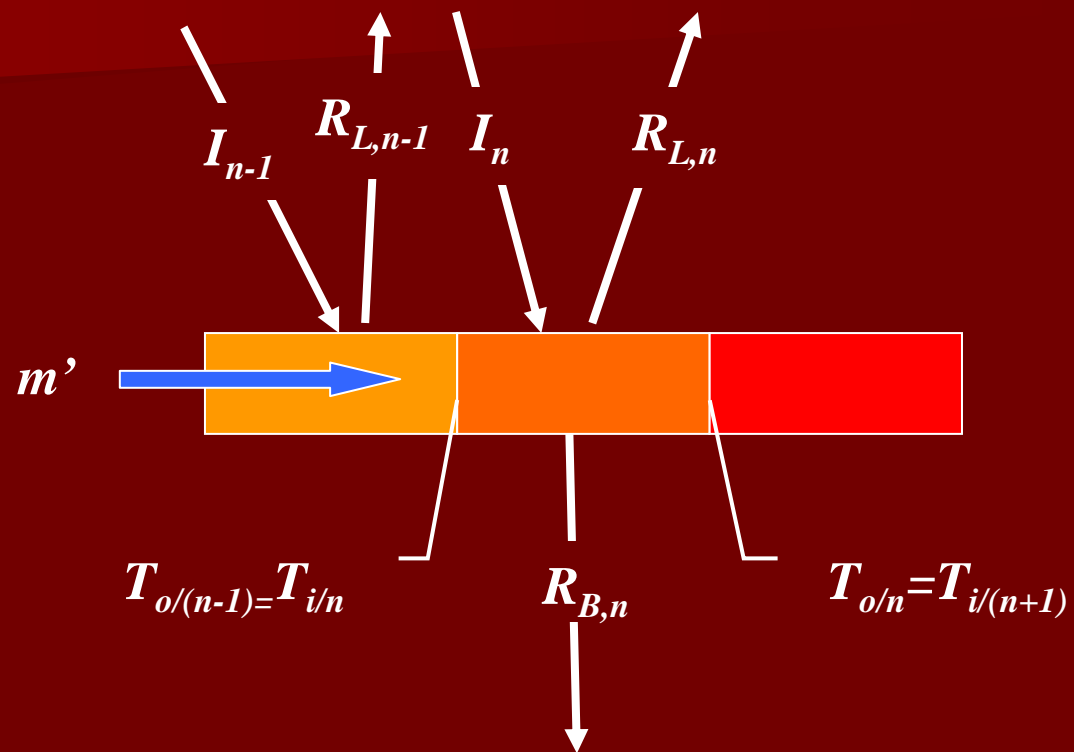
Energy balance equations in this model are :

$$\text{at collector : } E_{Sun} + E_{T \rightarrow C} = E_{lossC} + E_{C \rightarrow T}$$

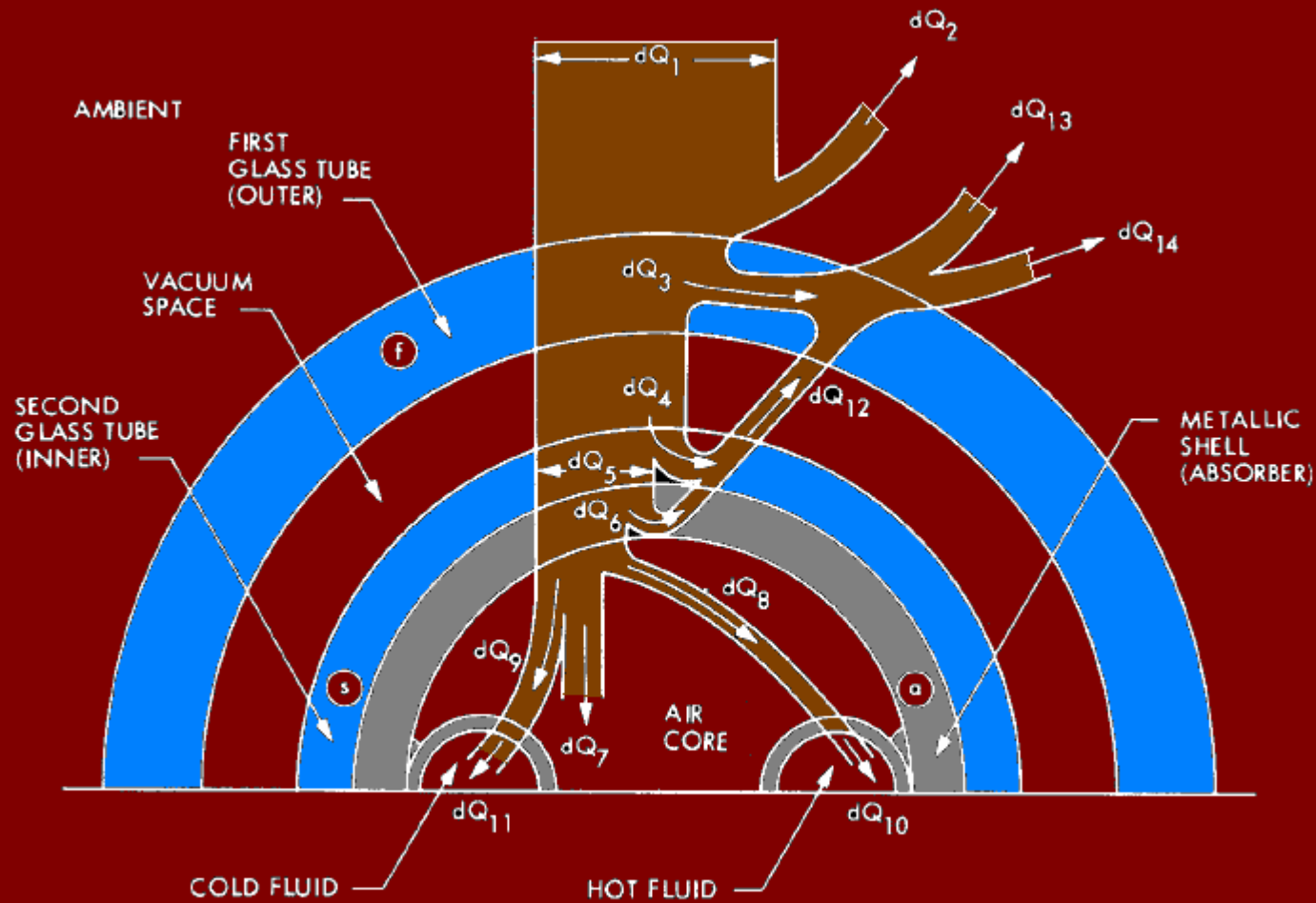
where  $E_{Sun}$  is power from sun (input power)(W) ,  $E_{T \rightarrow C}$  is power from storage tank to collector associated with water recycle(W) ,  $E_{lossC}$  is power losses due to imperfectly thermal insulation in collector (W) ,  $E_{C \rightarrow T}$  is power from collector to storage tank(W)

$$\text{at storage tank : } E_{C \rightarrow T} = E_{loss(T)} + E_{T \rightarrow U} + E_{T \rightarrow C}$$

# Energy balance in „Cell“ level:

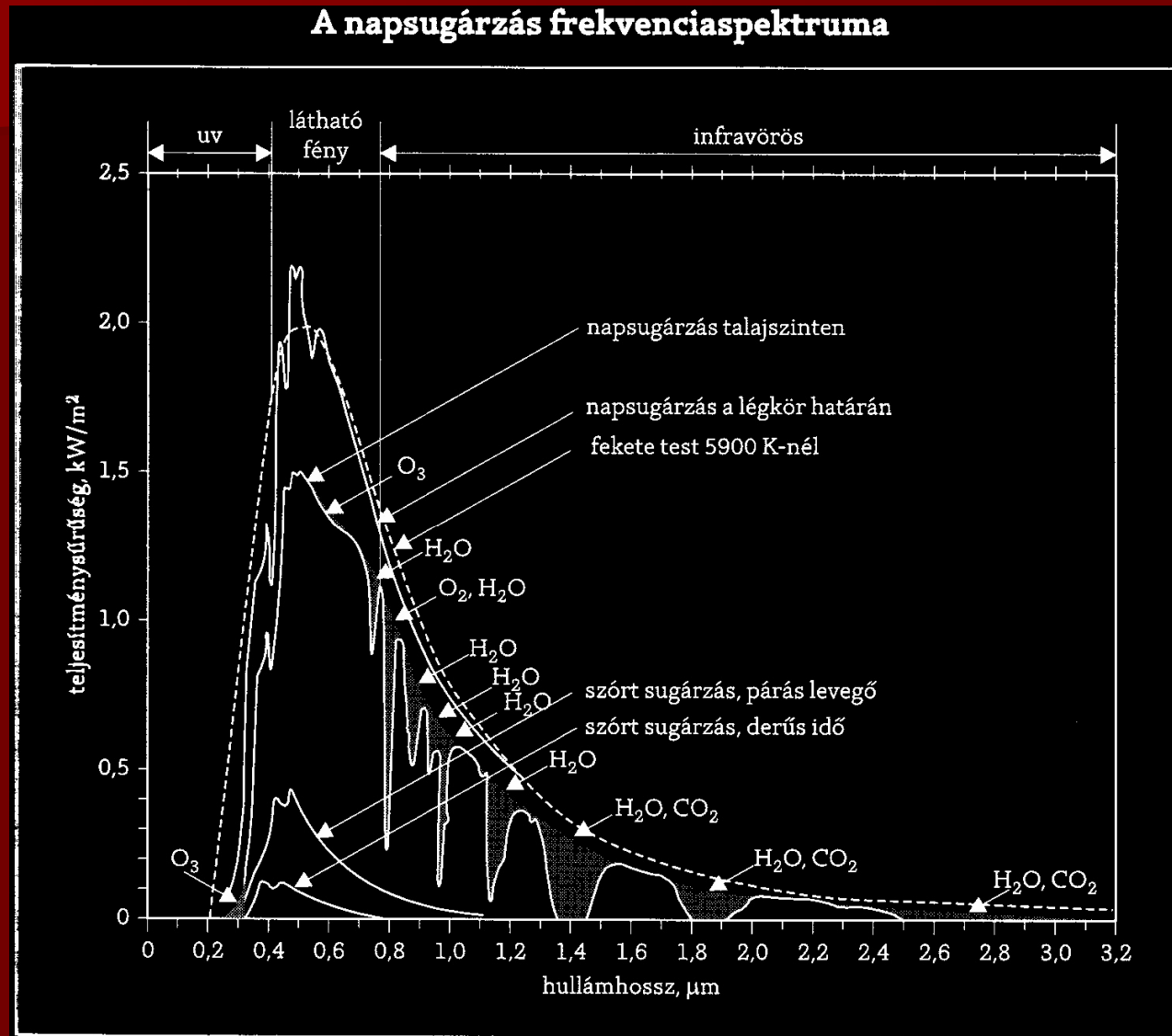


# Energy balance:



Sankey diagram for a twin tubular collector

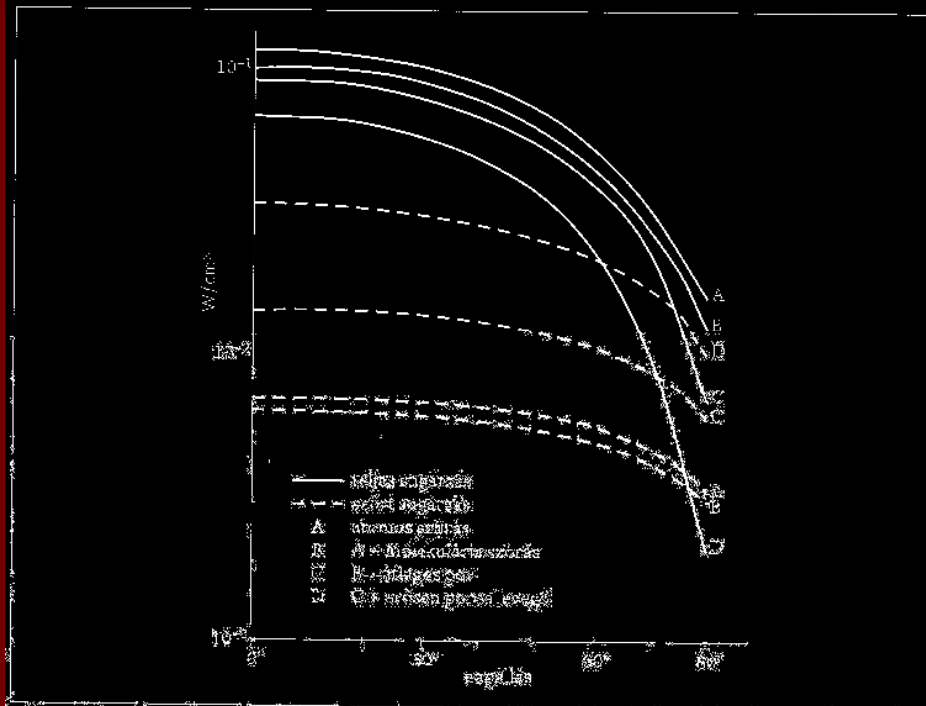
# Input data (1):



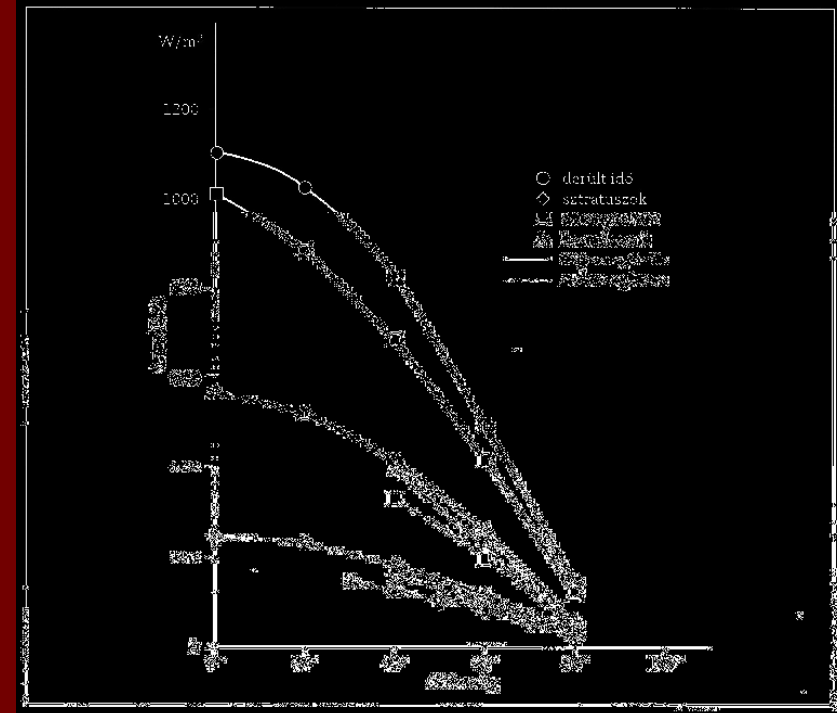


# Input data (2):

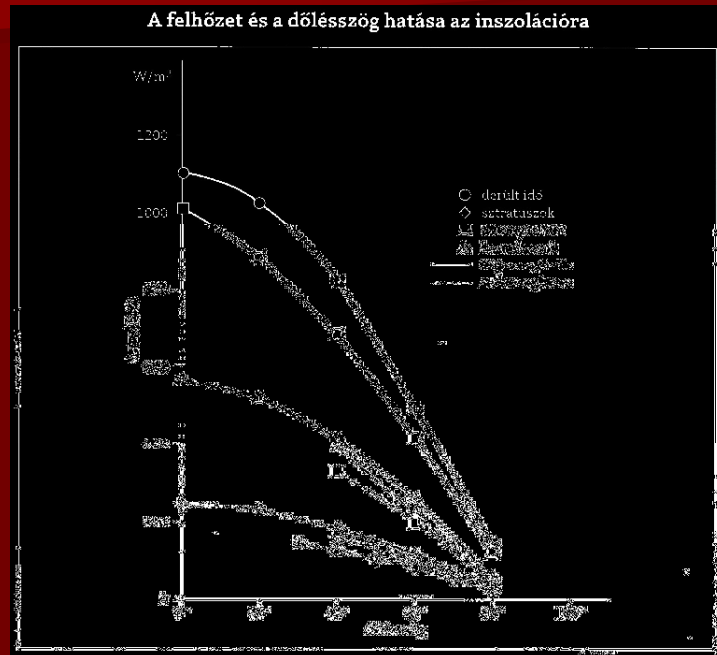
### Közvetlen és diffúz sugárzás modellezése



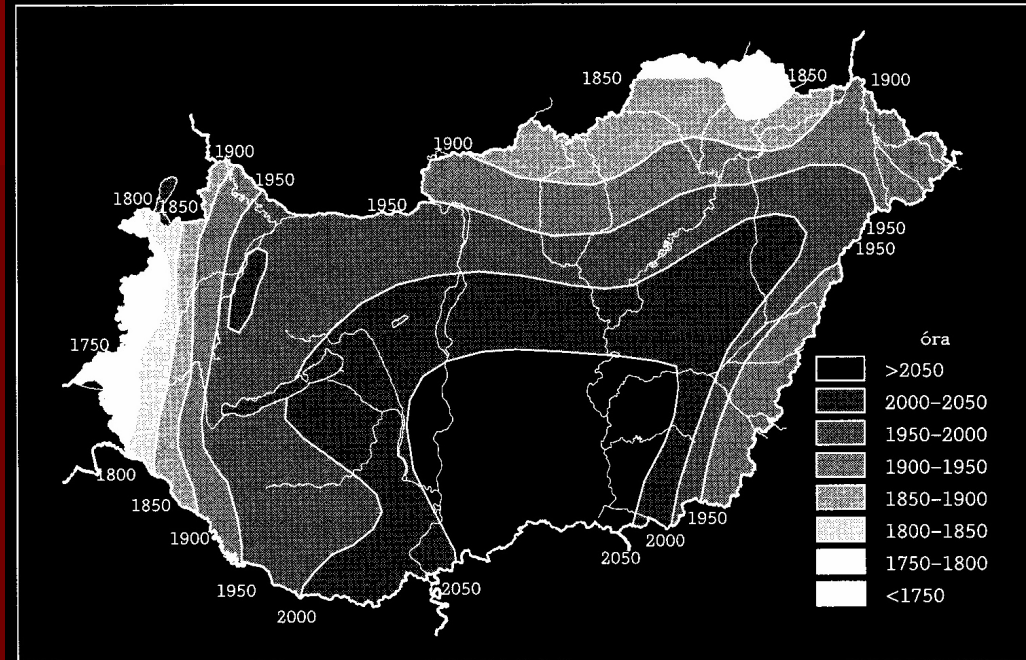
### A felhőzet és a dőlésszög hatása az inszolációra



# Input data(3):



## A napsütéstartam évi összegének területi megoszlása Magyarországon

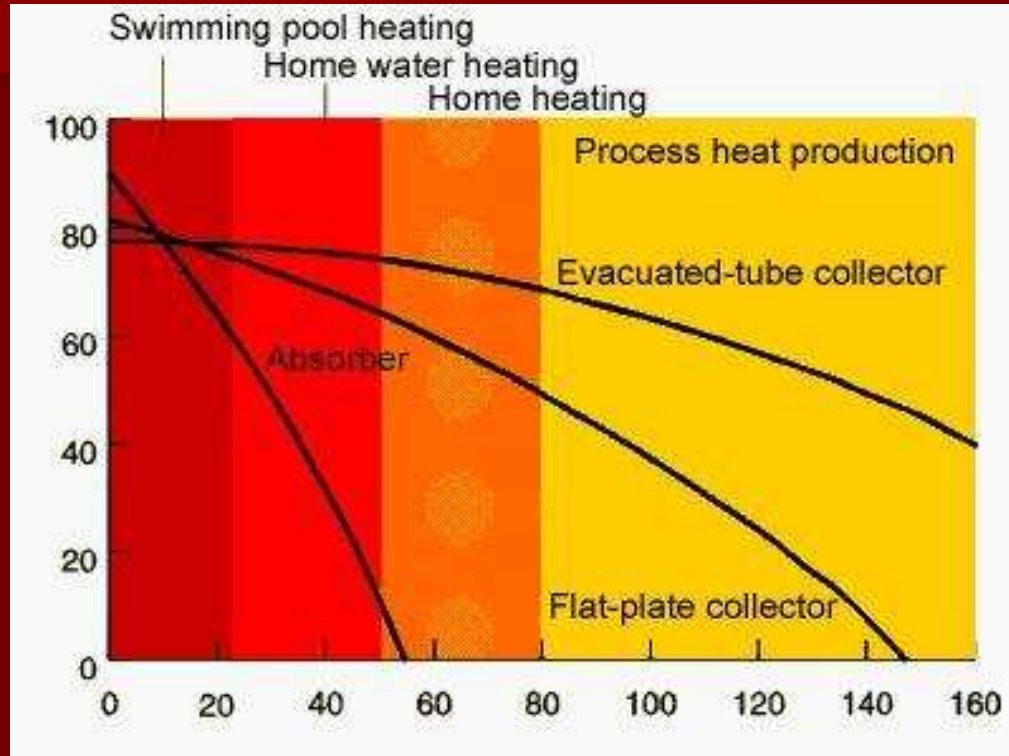


6. táblázat

### Napos órák havi és évi átlaga

		Hónapok											Éves átlag	
		I.	II.	III.	IV.	V.	VI.	VII.	VIII.	IX.	X.	XI.		XII.
napos órák	Budapest	55	84	137	182	230	248	274	255	197	156	67	48	1933
időtartama	Pécs	68	91	146	187	237	259	293	268	206	165	82	59	2061
energia, MJ/m <sup>2</sup>	Budapest	111	177	330	438	598	630	650	570	421	270	121	88	4406
	Pécs	120	187	340	476	615	640	660	580	410	270	132	94	4524

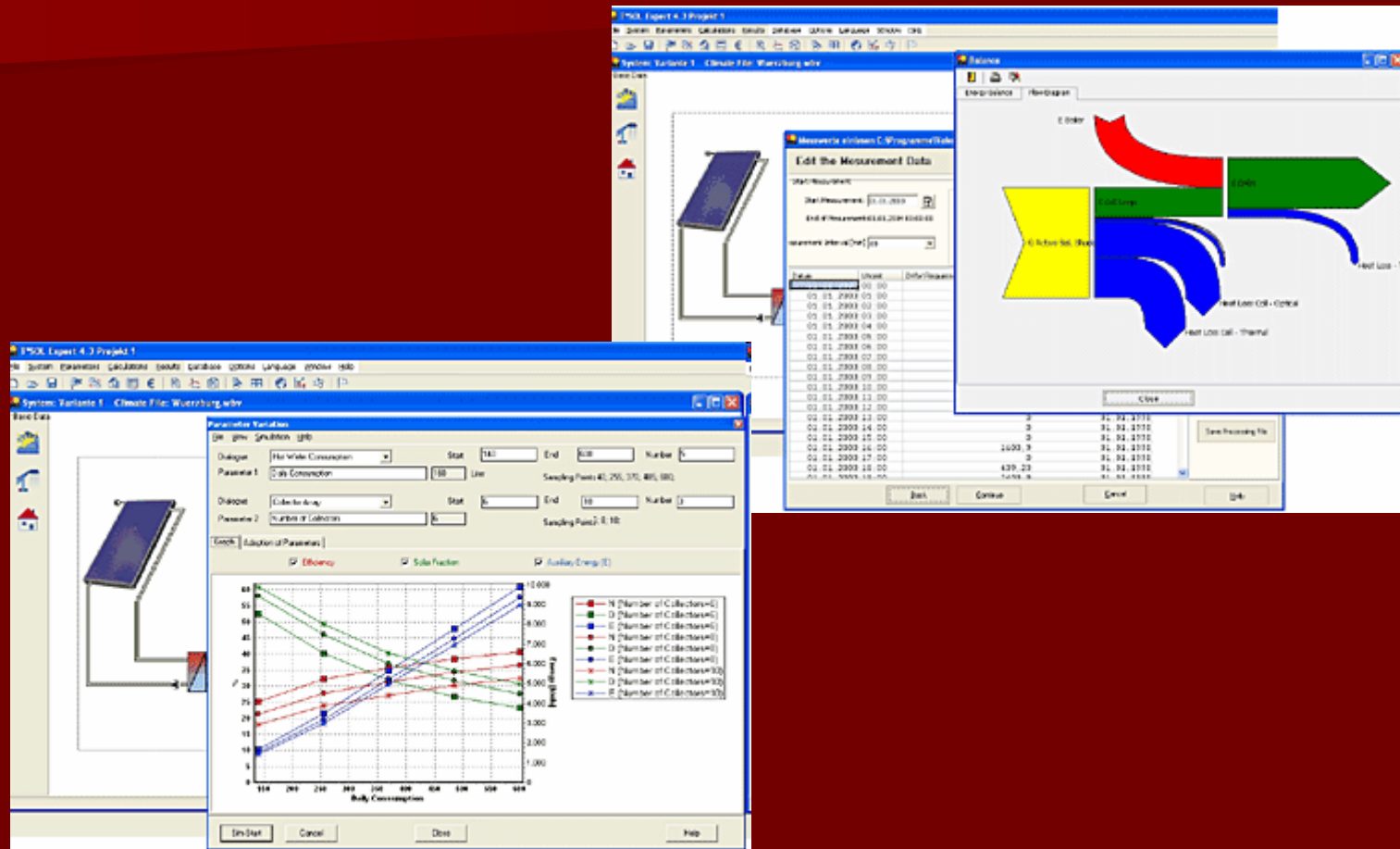
# General energy efficiency



$$\eta = \eta_0 - a_1 X - I \cdot a_2 X^2$$

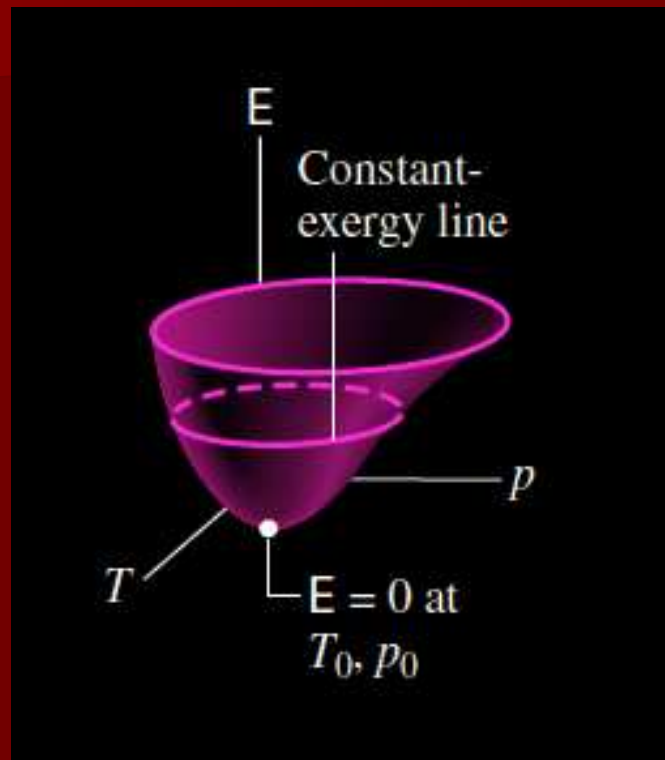
$$\eta_t = \frac{\int_{time} \dot{W}(\tau) \cdot \Delta T(\tau) \cdot d\tau}{\int_{time} A_I \cdot I(\tau) \cdot d\tau}$$

# Simulation softwares



# Exergy method:

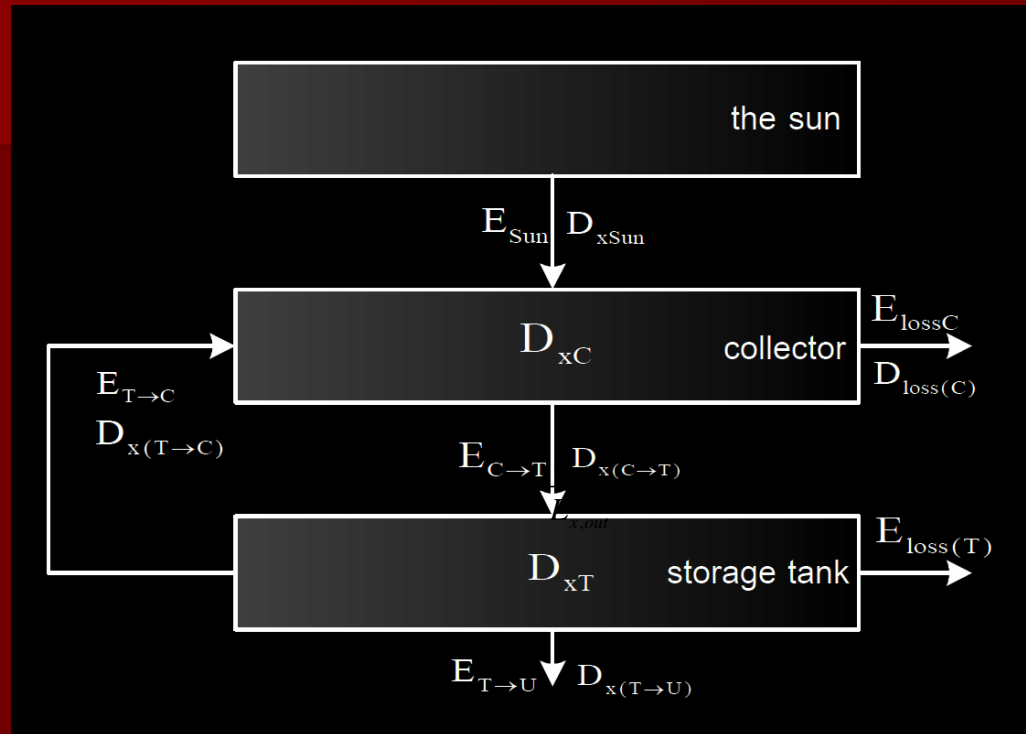
- Calculating the usable part of energy -

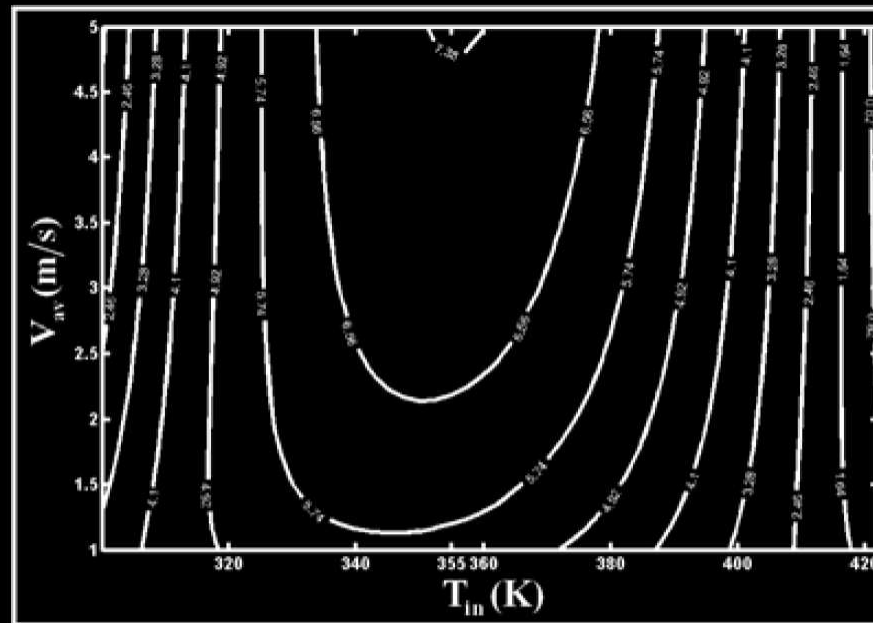


$$e = [(u + V^2/2 + gz) - u_0] + p_0(v - v_0) - T_0(s - s_0)$$

$$\left[ \begin{array}{l} \text{exergy transfer} \\ \text{accompanying heat} \end{array} \right] = \int_1^2 \left( 1 - \frac{T_0}{T_b} \right) \delta Q$$

# Exergy flow:

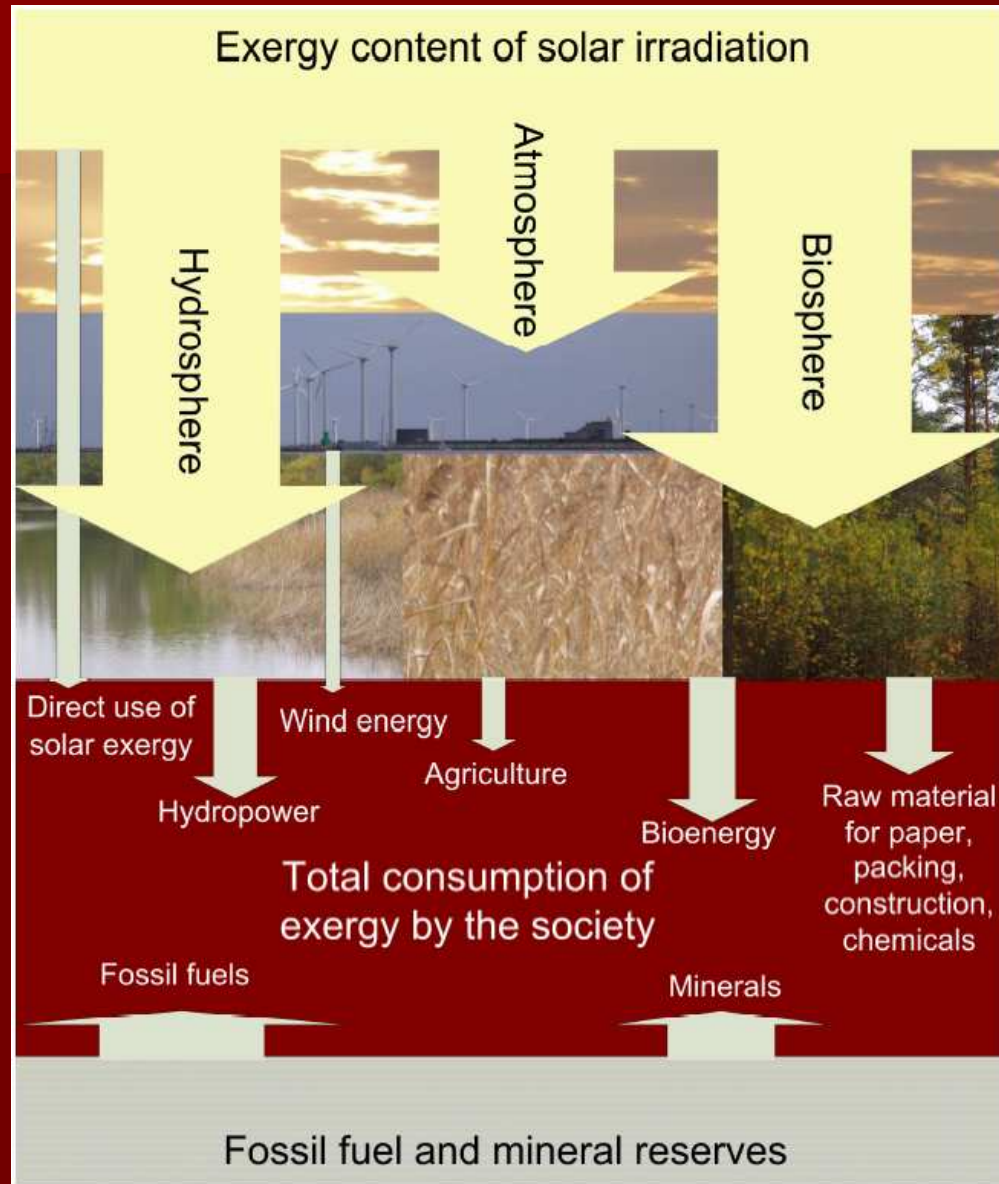




*Exergy efficiency contour  
according to average air velocity and fluid inlet*

$$\eta_E = 1 - \left\{ (1 - \eta_o) + \frac{\eta_o T_a (1/T_p - 1/T_s)}{(1 - T_a/T_s)} + \frac{U_l (T_p - T_a) (1 - T_a/T_p)}{I_T (1 - T_a/T_s)} + \frac{\dot{m} \Delta P T_a}{\rho T_m I_T A_p (1 - T_a/T_s)} + \frac{\eta_{th} T_a (1/T_m - 1/T_p)}{(1 - T_a/T_s)} \right\}$$

„Think about destroying exergy during using energy“





The *performance of a solar heating system* depends on

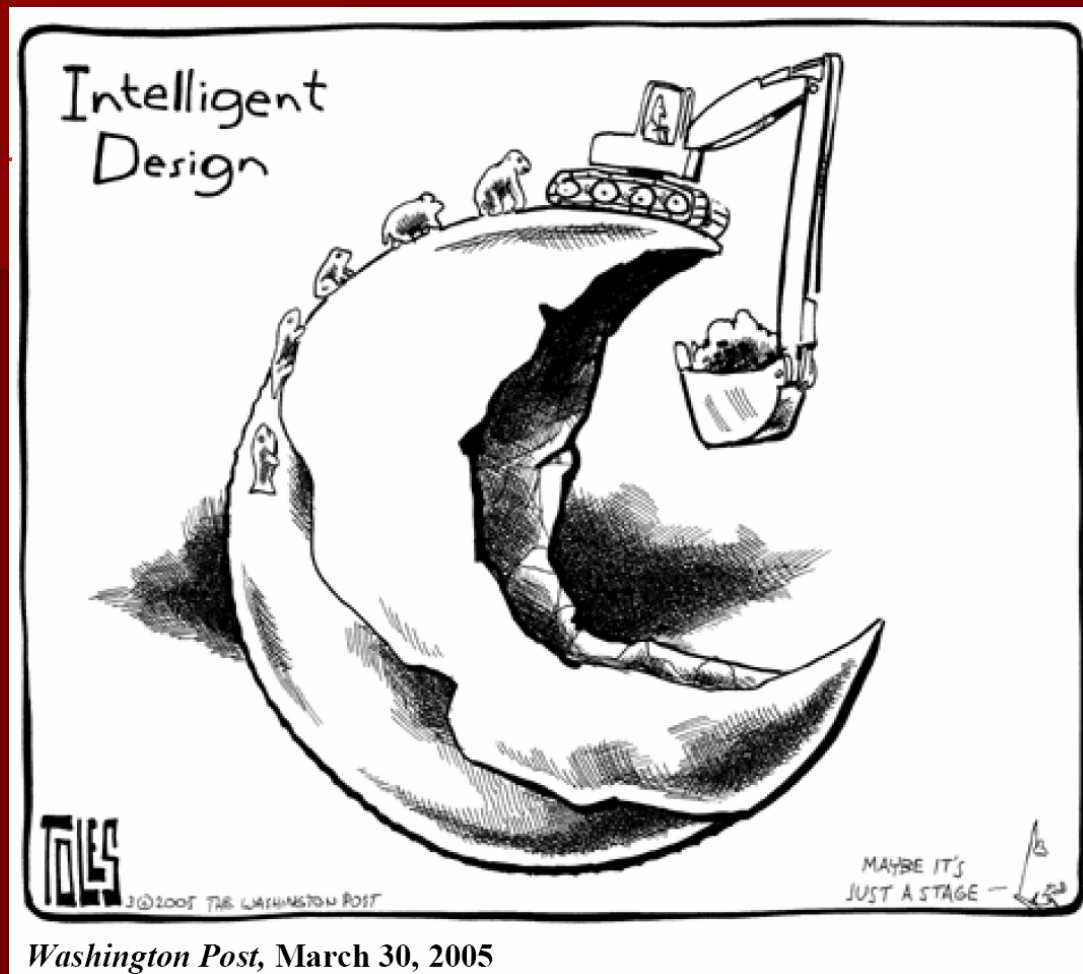
✓ the *local climatic conditions*

✓ the *collector area and type*

the overall annual performance of a solar system is technically limited by the amount of energy that can be collected during the winter time. Improvements in collector design can also have a significant effect on the overall system performance.

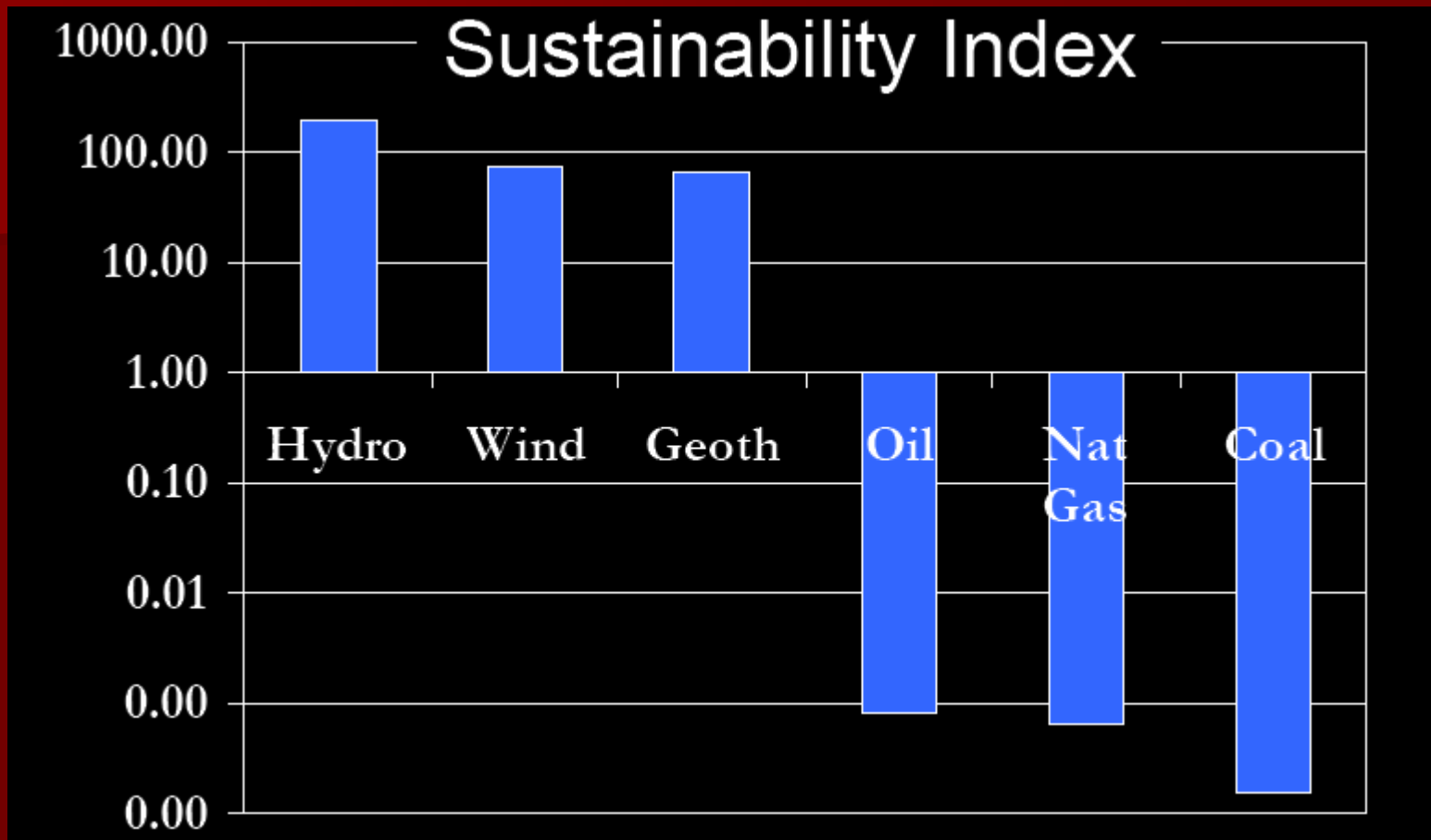
✓ the *temperature levels*

the *delivery temperature* and the *cold water supply temperature*.



*Washington Post*, March 30, 2005

Thank you for attention!



$$\text{Sustainability Index} = \frac{\text{Return on Exergetic Investment}}{\text{Environmental load}}$$